

$$-\int_{T_0}^{T_1} \bar{q} \frac{dz}{dT} dT = \bar{q}L$$

$$\frac{dT}{d(\bar{q} - q_c)^2} \quad (26)$$

or the variation of the temperature substituted into (14) to yield

$$\frac{dT}{d(\bar{q} - q_c)^2} \quad (27)$$

obtain comparisons with the experi-

be easily altered in order to arrive pressure in circular capillaries. For a ely replaced by $3r^2/2$.

(11) is a good one. We investigate

$$\frac{\beta/dz^2}{\bar{q}^{-1}(d^2q/dx^2)} \quad (28)$$

re range of interest ($1.15^\circ < T < n \sim 5.6$). Let $T/T_\lambda = \zeta$ and $\beta_\lambda =$

$$\beta_\lambda \zeta^{-(n+2)} \frac{d\zeta}{dz} \quad (29)$$

$$\left[\zeta^{-(n+2)} \frac{d^2\zeta}{dz^2} \right] \quad (30)$$

$$\alpha d^2\bar{q}^3(4n+5-2\zeta^n-4n\zeta^n)] \quad (31)$$

$$+ \alpha d^2\bar{q}^3) \quad (32)$$

$$\left(\frac{4+2-2\zeta^2-4n\zeta^n}{\zeta(1-\zeta^n)} \right) \frac{d\zeta}{dz} \quad (32)$$

From (12) and (13) we obtain the other required coefficient:

$$\frac{d^2q}{dx^2} = -\frac{12\bar{q}}{d^2} \quad (33)$$

The work of Khalatnikov (8) has indicated that the bulk viscosity may be of the order of ten times the ordinary viscosity, so in estimating an upper limit on R_1 we consider the viscosity term to be $\frac{1}{12}$. Also, the maximum value of q is $\frac{3}{2}\bar{q}$. Substituting (30) and (33) into (28) we obtain an expression for R_1 in terms of known or calculable quantities. For $d = 2\mu$ and the maximum q 's encountered in these experiments, Table I presents the maximum value attained by R_1 at several temperatures, from which it is seen that in these experiments $R_1 \ll 1$.

The ratio of the pressure gradients R_p across the slit to those along it may be found from (9) and (10), neglecting the small second term in (9).

$$R_p = \frac{\partial P/\partial x}{\partial P/\partial z} = \left(\frac{\eta_n + \eta'}{\eta_n} \right) \frac{(dq/dx)(d\beta/dz)}{\beta(d^2q/dx^2)} \quad (34)$$

Estimates of the maximum values of R_p are also given in Table I and indicate that except for the largest heat flows in the vicinity of the λ -point the pressure gradient across the slit is negligible compared to that along the slit. By virtue of the relation (16) between ∇P and ∇T the same statement may be made for the temperature gradient, indicating the extent of validity for the assumption made in (8) that T is a function of z alone.

The second order terms in (1) and (2) may be shown to be small in the same way. We are concerned with gradients of the energy in the z direction. In (2) we compare the z component of the left hand side with the z component of ∇P :

$$R_E = \frac{\rho_n[\partial(v_n^2/2)/\partial z]}{(\rho_n/\rho)\partial P/\partial z} = \frac{\rho(d/dz)(\beta^2\bar{q}^2)}{(24\eta_n\bar{q})/(\rho sTd^2)} \quad (35)$$

Since

$$\beta^2 = \beta_\lambda^2 \zeta^{-2(n+1)}, \quad R_E \sim (n+1)\rho\beta^3\bar{q}^2(1 + \alpha d^2\bar{q}^2). \quad (36)$$

TABLE I
MAXIMUM VALUES OF THE RATIOS R_1 , R_p , AND R_E CORRESPONDING TO THE MAXIMUM HEAT CURRENT DENSITY \bar{q}_{\max} AT SEVERAL TEMPERATURES FOR SLIT I ($d = 2\mu$), $T_0 = 1.1^\circ\text{K}$

$T(^{\circ}\text{K})$	Λ (watt/ $\text{cm}^3 - \text{deg}$)	α ($\text{cm}^2/\text{watt}^2$)	\bar{q} (watt/ cm^2)	R_1	R_p	R_E
1.2	3×10^6	6.9×10^5	10^{-1}	$<10^{-4}$	4×10^{-3}	10^{-3}
1.8	7.3×10^8	5.2×10^5	10	$<10^{-5}$	4×10^{-3}	9×10^{-3}
2.15	3.5×10^9	3.3×10^7	15	$<10^{-6}$	$<10^{-1}$	3×10^{-2}